Nuclear Optical Model Analysis of Neutron Elastic Scattering for Calcium*

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A nuclear optical model calculation of neutron elastic scattering using five parameters has been made. Appropriate estimates of the effect of compound elastic scattering at low energies are included. Comparisons have been made with experimental data, and results for the parameters adopted are given for elastic scattering in the energy range from 0.734 to 18 Mev. Although reasonably good agreement between the calculation and experimental results have been obtained, there is a discrepancy between experiments below 2 Mev, and experimental data is needed between 6 and 14 Mev. Both angular distributions and Legendre expansion coefficients for the total elastic scattering are given.

1. Introduction

The nuclear optical model has been outstandingly successful in describing the elastic scattering of neutrons and other nuclear particles above the energy of perhaps 6 Mev, where compound elastic scattering processes are not important. Below these energies it is necessary to include some estimate of compound elastic scattering. At neutron energies below the first excited state of the target nucleus, inclustic scattering is not possible. In this energy range it is possible to describe the compound elastic scattering by use of the fluctuation cross section (Feshbach, 1960). Above this energy the angular distribution of the compound elastic scattering may be obtained from the compound statistical model [Hauser and Feshbach, 1952].

Initially in the present work the experimental data was analyzed using the six-parameter nuclear optical model of Bjorklund and Fernbach [1958]. However, it was found that at least as good fits to the experimental data could be obtained with a five-parameter model, using derivative surface absorption instead of an adjustable parameter to determine the width of the imaginary (absorptive) well. This latter model, which contains a Saxon real potential, a Thomas spin-orbit potential, and a surface imaginary poten-

tial, was used in this calculation.

This calculation is the first of a series which will provide data in a form suitable for input to neutron penetration calculations with digital computers. The present calculations are for calcium, an important component of concrete which is widely used for neutron shielding. Comparisons with experimental elastic scattering angular distributions are included. Angular distributions and Legendre coefficients for the calculated angular distributions are both presented. The calculations have been programed in Fortran for the IBM 7090 computer at the National Bureau of Standards.

2. Description of the Calculation

2.I. Solution of the Wave Equation

Although the exact phase shift analysis carried out here is standard in many respects, it seems desirable to record the specific method of calculation, including the Legendre polynomial analysis.

We start with the radial part of the non-relativ-

istic Schrödinger wave equation:

$$\frac{d^{2}U_{l}(r)}{dr^{2}} + \frac{2m}{\hbar^{2}} \left[E - \frac{l(l+1)\hbar^{2}}{2mr^{2}} - (V(r) + iW(r)) \right] \times U_{l}(r) = 0. \quad (1)$$

The potential is described by V(r)+iW(r) where V(r) is the real part of the potential and W(r) is the imaginary part. The wave function $U_t(r)$ will also have both real and imaginary parts:

$$U_t(r) = X_t(r) + iY_t(r). \tag{2}$$

Equation (1) becomes:

$$\frac{d^{2}(X_{t}+iY_{t})}{dr^{2}} + \frac{2m}{\hbar^{2}} \left[E - \frac{l(l+1)\hbar^{2}}{2mr^{2}} - V - iW \right] \times (X_{t}+iY_{t}) = 0. \quad (3)$$

Separating this equation into real and imaginary parts, we obtain two coupled real equations which may be solved on the computer.

$$\frac{d^2X_1}{dr^2} + \frac{2m}{\hbar^2} \left[E - \frac{l(l+1)\hbar^2}{2mr^2} - V \right] X_t + \frac{2m}{\hbar^2} WY_t = 0 \quad (4)$$

$$\frac{d^{2}Y_{i}}{dr^{2}} + \frac{2m}{\hbar^{2}} \left[E - \frac{l(l+1)\hbar^{2}}{2mr^{2}} - V \right] Y_{i} - \frac{2m}{\hbar^{2}} W X_{i} = 0. \quad (5)$$

These equations are integrated step-by-step outward in radius by the second order Runge-Kutta method [see, for example, Zurmühl, 1961]. The number of

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integration steps is typically 100 to 500. If the wave functions become large, they are automatically renormalized to smaller values by the code. The running time for 15 l's and 200 steps is about 1 min per energy including all angular distributions. The mass appearing in these equations is the reduced mass of the neutron in the neutron-nucleus center-of-mass system. The energy, E, is that of the neutron in the center-of-mass system. When the complex potential (V+iW) approaches a non-vanishing constant at the origin, then

$$U_1(r) \rightarrow C_1 r^{l+1} \text{ as } r \rightarrow 0$$
 (6)

where C_t is a complex number independent of r [Amster, Leshan, and Walt, 1960]. In the presence of the spin-orbit term (see below) there is a 1/r behavior of the potential energy for small values of r; however, eq (6) still holds since this term is dominated by the $1/r^3$ dependence of the centrifugal potential [see Bohm, 1951]. Since the cross sections depend only on the logarithmic derivative of the wave function, the normalization is arbitrary and C_t can be taken to be any non-zero value. We have chosen k(1+i) for C_t where k is a small number chosen to prevent underflow or overflow problems. Provision is made in the code to calculate for values of l up to l=29.

For the optical model parameters we have used a potential whose real and imaginary parts are:

$$V(r) = V_{\epsilon} \rho(r) - \alpha V_{\epsilon} \left(\frac{\hbar}{2Mc}\right)^{2} (\overrightarrow{l} \cdot \overrightarrow{\sigma}) \frac{1}{r} \frac{d\rho}{dr}, \quad (7)$$

$$W(r) = W_s \left(4a \frac{d\rho}{dr} \right) = W_s \left(4\rho^2 \exp \left[\frac{r - R_0}{a} \right] \right) \quad (8)$$

where

$$\rho(r) = \frac{1}{1 + \exp\left[\frac{r - R_0}{a}\right]}$$

the usual "Saxon" potential; α is the strength of the spin-orbit interaction relative to the "Thomas" term for a nucleon; M is the neutron mass; V_c is the central real potential; W_t is the lowest value of the imaginary surface potential; $\frac{\hbar}{Mc}$ is the Compton

wavelength for a nucleon; \vec{l} is the orbital angular momentum of the neutron; $\vec{\sigma}$ is the Pauli spin operator of the incident neutron; R_0 is the nuclear radius; and \vec{a} is the "diffuseness" parameter of the real potential. If the spin angular momentum of the incident neutron is parallel to the orbital angular momentum of the incident neutron, then j=l+1/2, and $\vec{\sigma} \cdot \vec{l} = l$. If the spin and orbital angular momentum are anti-parallel, then j=l-1/2 and $\vec{\sigma} \cdot \vec{l} = -(l+1)$. This leads to two real potentials, $V^+(r)$ and $V^-(r)$ corresponding to the parallel and anti-parallel $\vec{\sigma} \cdot \vec{l}$ interactions. The wave equation is solved for each of these. To obtain the desired

cross sections, we need the phase shifts η_i^+ and η_i^- which measure the effect of the complex potential on the neutron partial waves. These phase shifts are obtained by a calculation which compares the value for logarithmic derivative f_i obtained by numerical integration in the presence of the nuclear potential with the corresponding quantity $(\Delta_i + iS_i)$ for the zero phase shift spherical Hankel function solutions obtained in the absence of the nuclear potential.

The required expression for η_i is given by Blatt and Weisskopf [1952]:

$$\eta_{i} = \frac{f_{i} - \Delta_{t} + iS_{t}}{f_{t} - \Delta_{t} - iS_{t}} \exp(2i\xi_{t}). \tag{9}$$

For neutrons

$$\exp (2i\xi_{l}) = \frac{G_{l}(R) - iF_{l}(R)}{G_{l}(R) + iF_{l}(R)}, \quad (10)$$

where $G_i(R)$ and $F_i(R)$ are solutions of eq. (1) with (V(r)+iW(r))=0. In terms of spherical Bessel functions, $F_i(x)=xj_i(x)$ and $G_i(x)=xn_i(x)$ where x=kR.

2.2. Evaluation of the Cross Sections Directly From the Nuclear Optical Model

The total cross section predicted by the nuclear optical model is made up of a shape-elastic scattering cross section and a compound nucleus formation cross section [Feshbach, Porter, and Weisskopf, 1954]:

$$\sigma_i = \sigma_e + \sigma_e$$
.

However, the compound nucleus may decay into the entrance channel producing "compound elastic" scattering or it may produce inelastic scattering or charged particle reactions:

$$\sigma_c = \sigma_{cc} + \sigma_{cc}$$

These equations may now be rearranged to separate the elastic scattering (σ_{ss} and σ_{cs} are not distinguishable experimentally) from the reaction cross section:

$$\sigma_e = (\sigma_{ee} + \sigma_{ee}) + \sigma_r = \sigma_e + \sigma_r.$$

In the present calculation σ_{te} is estimated by the "fluctuation" cross section, σ_{ft} , which is important below energies of about 6 Mev:

$$\sigma_t = \sigma_{ss} + \sigma_{fl} + \sigma_r$$

When inelastic scattering and reactions are zero or negligible, the entire cross section is elastic:

$$\sigma_1 = \sigma_{aa} + \sigma_{rb}$$

In this case the fluctuation cross section may be obtained very simply from the phase shifts of the optical model alone (see Feshbach [1960] for a discussion of the fluctuation cross section).

We now proceed to evaluate the various cross sections from the calculated phase shifts (η_i) . For both incident particles and the nucleus without spin, the expressions for the incident plane wave, the total wave (which shows the effect of the potential of the nucleus on the incident wave), and the scattered wave are:

$$e^{ikz} = \sum_{l=0}^{\infty} i^{l} \frac{2l+1}{2} \left[h_{l}^{*}(kr) + h_{l}(kr) \right] P_{l}(\cos\theta), \quad (11)$$

$$\psi_{tot}(r) = \sum_{l=0}^{\infty} i^{l} \frac{2l+1}{2} \left[h_{l}^{\bullet}(kr) + \eta_{l} h_{l}(kr) \right] P_{t}(\cos \theta), \quad (12)$$

and

 $\psi_{\text{accats}}(r) = \psi_{\text{tot}}(r) - e^{ikz}$ $= \sum_{l=0}^{\infty} i^{l} \frac{2l+1}{2} (\eta_{l} - 1) h_{l}(kr) P_{l}(\cos \theta). \quad (13)$

The incident neutrons which have spin 1/2 may be represented by a plane wave;

$$\psi_{\rm ms} = e^{ikz} \chi_{\rm ins} \tag{14}$$

where χ_{inc} describes the spin wave function of the neutron. $\chi_{\text{inc}} = \binom{0}{0}$ is spin "up." $\chi_{\text{inc}} = \binom{0}{1}$ corresponds to spin "down." In the presence of the nuclear potential the asymptotic form of the wave function of the neutron is:

$$\psi \longrightarrow \psi_{\rm inc} + \frac{1}{r} e^{itr} F(\theta) \chi_{\rm inc} \qquad (15)$$

where $F(\theta)$ is the scattering matrix.

$$F(\theta) = A(\theta) + B(\theta) \stackrel{\longrightarrow}{\sigma \cdot n} \tag{16}$$

where n is a unit vector perpendicular to the plane of scattering. According to the Basel convention [Huber and Meyer, 1961], the positive direction of polarization, given by the unit vector n, is:

$$\vec{n} = \frac{\vec{k}_t \times \vec{k}_f}{|\vec{k}_t \times \vec{k}_f|} \tag{17}$$

where \vec{k}_i and \vec{k}_f are the wave vectors of the incident and scattered neutrons.

In the equations above, $h_i^*=j_i-in_i$ and represents an incoming spherical wave and $h_i=j_i+in_i$ and represents an outgoing spherical wave. To extend this treatment to the case of neutrons with spin incident on spin-zero nuclei [Lepore, 1950], we introduce the operators π_i^* and π_i^- which select the states for which $j=l+\frac{1}{2}$ and $j=l-\frac{1}{2}$, respectively. These operators are

$$\boldsymbol{\pi}_{l}^{+} = \frac{l+1+\overrightarrow{\sigma \cdot l}}{2l+1} \text{ and } \boldsymbol{\pi}_{l}^{-} = \frac{l-\overrightarrow{\sigma \cdot l}}{2l+1}.$$
 (17a)

If $j=l+\frac{1}{2}$, $\pi^{+}=1$, $\pi^{-}=0$. If $j=l-\frac{1}{2}$, $\pi^{+}=0$, $\pi^{-}=1$. Applying our operators to the total wave function, eq (16) we have

$$\psi_{\text{tot}} = \sum_{l=0}^{\infty} \frac{2l+1}{2} i^{l} [\pi^{+} + \pi^{-}] [h_{l}^{*}(k\tau) + \eta_{l}h_{l}(k\tau)] \times P_{l}(\cos\theta) \chi_{\text{inc}}, \quad (17b)$$

Let η_i^+ and η_i^- be phase shifts corresponding to the parallel and anti-parallel spin-orbit orientations for the neutron. At large radii we use the asymptotic form of the Hankel functions,

$$\begin{aligned} \psi_{tot} = & \sum_{i=0}^{\infty} \frac{(2i+1)i^{i}}{2k\tau} \left\{ \pi_{i}^{+} \left(\pi_{i}^{+} e^{i \left[k\tau - (i+1) \frac{\pi}{2} \right]} \right) + e^{-i \left[k\tau - (i+1) \frac{\pi}{2} \right]} \right) + \pi_{i}^{-} \left(\pi_{i}^{-} e^{i \left[k\tau - (i+1) \frac{\pi}{2} \right]} \right) \\ & + e^{-i \left[k\tau - (i+1) \frac{\pi}{2} \right]} \right) \right\} \times P_{t}(\cos \theta) \chi_{loc}. \end{aligned}$$
(17c)

If we now subtract the incident wave from the total wave to obtain the scattered wave, we find

$$\Psi_{\text{seatt}} = \sum_{l=0}^{\infty} \frac{e^{ikt}}{2ikr} \left[(l+1)(\eta_l^+ - 1) + l(\eta_l^- - 1) + (\eta_l^+ - \eta_l^-) \overrightarrow{\sigma \cdot l} \right] P_t(\cos\theta) \chi_{\text{inc}}, \quad (18)$$

where we have used the expressions (17a) for the operators and the condition that when $\eta_I^+ = \eta_I^- = 1$, ψ_{scatt} must equal zero. The right-left asymmetry in the scattering of a polarized beam is introduced through the $(\sigma \cdot \vec{l})$ operator:

$$(\overrightarrow{\sigma \cdot l})P_i(\cos\theta) = \overrightarrow{\sigma} \cdot \left[\overrightarrow{n}\left(-i\frac{\partial}{\partial \theta}\right)P_i(\cos\theta)\right]. \quad (19)$$

However, $\frac{\partial}{\partial \theta} = -\sin \theta \frac{\partial}{\partial (\cos \theta)}$. Finally,

$$(\vec{\sigma} \cdot \vec{l}) P_t(\cos \theta) = (\vec{\sigma} \cdot \vec{n}) \left[i \sin \theta \frac{\delta}{\delta (\cos \theta)} P_t(\cos \theta) \right], \tag{20}$$

$$(\vec{\sigma} \cdot \vec{l})P_i(\cos \theta) = (\vec{\sigma} \cdot \vec{n})iP_i(\cos \theta). \tag{21}$$

where $P_i^i(\cos \theta) = \sin \theta \frac{\delta}{\delta(\cos \theta)} P_i(\cos \theta)$. Note: a $(-1)^m$ term is sometimes included in the definition of the associated Legendre function $P_i^m(\cos \theta)$, in which case our function has the opposite sign, and a minus sign appears on the right side of eq (21). $A(\theta)$ and $B(\theta)$ appearing in the scattering matrix, eq (16) are:

$$A(\theta) = \frac{1}{2ik} \sum_{l=0}^{\infty} \left[(l+1)(\eta_l^+ - 1) + l(\eta_l^- - 1) \right] P_l(\cos \theta)$$
(22)

$$B(\theta) = \frac{1}{2k} \sum_{i=1}^{\infty} \{\eta_i^+ - \eta_i^-\} P_i^{\dagger}(\cos \theta). \tag{23}$$

The differential scattering cross section is

$$\frac{d\sigma}{d\Omega} = \frac{1}{2} tr F^{+} F = |A|^{2} + |B|^{2}.$$
 (24)

The polarization is given by

$$P = \frac{2 \text{ Re } (A^*B)}{|A|^2 + |B|^2}.$$
 (25)

For a completely polarized incident beam with spin "up," P=(L-R)/(L+R), where L and R are the measured left and right detector counting rates.

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shape elastic cross sections (integrated over angle)

$$\sigma_{l} = \frac{\pi}{k^{2}} \sum_{l=0}^{\infty} \left[(l+1)2 \operatorname{Re} \left(1 - \eta_{l}^{+} \right) + l 2 \operatorname{Re} \left(1 - \eta_{l}^{-} \right) \right]$$
 (26)

$$\sigma_{e} = \frac{\pi}{k^{2}} \sum_{l=0}^{\infty} \left[(l+1) \left(1 - |\eta_{l}^{+}|^{2} \right) + l \left(1 - |\eta_{l}^{-}|^{2} \right) \right]$$
 (27)

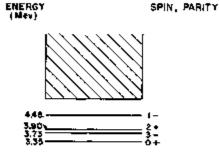
$$\sigma_{ts} = \frac{\pi}{k^3} \sum_{l=0}^{\infty} \left[(l+1)|1 - \eta_l^+|^2 + l|1 - \eta_l^-|^2 \right]. \tag{28}$$

For use in inelastic scattering calculations and in our estimate of compound elastic scattering, the "transmission coefficients" are also calculated:

$$T_1^+ = (1 - |\eta_1^+|^2) \text{ and } T_1^- = (1 - |\eta_1^-|^2).$$
 (29)

2.3. Compound Elastic Scattering

Whereas shape elastic scattering is given directly by the nuclear optical model, our estimate of compound elastic scattering is treated in four different ways depending upon the incident neutron energy. Below 3.35 Mev, it may be obtained from the optical model phase shifts, with a small correction for the



Fraure 1. Low-lying energy levels of Ca*.

Spins and parities in parentheses are taken from Troubstakov, Kalos, Lustig, Ray, and Trupin [1961]. Levels taken as a continuum above 6 Mev.

observed (n, p) cross section. In the energy range from 3.35 to 5.0 Mev, a Hauser-Feshbach [1952] hand calculation using discrete energy levels of the target nucleus (see fig. 1) was made. From 5.0 to 5.7 Mev a Hauser-Feshbach calculation using a statistical-model residual nucleus was made. In this case the compound elastic scattering is isotropic because of the randomness of the spins and parities of the levels assumed in the statistical model. The angular isotropy has been proved by Wolfenstein [1951] and by Hauser and Feshbach. Above 6 Mev compound elastic scattering is neglected.

The fluctuation cross section, in the absence of inelastic scattering and reactions, may be obtained from the phase shifts of the optical model [Feshbach,

$$\begin{split} |A|_{I^{1}}^{2} = & \frac{1}{4k^{2}} \sum_{l=0}^{\infty} \left\{ (l+1)^{2} (1-|\eta_{l}^{+}|^{2})^{2} + l^{2} (1-|\eta_{l}^{-}|)^{2} \right\} \\ \times & \left[P_{l}(\cos\theta) \right]^{2} \end{split}$$

$$|B|_{II}^{2} = \frac{1}{4k^{2}} \sum_{l=1}^{\infty} \{ (1 - |\eta_{l}^{+}|^{2}) + (1 - |\eta_{l}^{-}|^{2}) \} [P_{i}^{i}(\cos\theta)]^{2}, \quad (30)$$

At energies below the energy of the first excited state in the target nucleus (3.35 Mev for Ca⁴⁰), we have used eq (30) to calculate the compound elastic scattering. Note that this leads not to isotropic scattering but to an angular distribution which goes predominantly as $[P_i(\cos \theta)]^2$ for neutrons of angular momentum t.

The cross section for inelastic scattering of a neutron of incident angular momentum I_i final angular momentum l', from a nucleus of initial angular momentum i and final angular momentum i'is given by Hauser and Feshbach as

$$\sigma(l, i|l', i') = \frac{1}{2(2i+1)} \sum_{\boldsymbol{a}, \boldsymbol{\theta}} \sigma(l, j_{\boldsymbol{a}}|l', j'_{\boldsymbol{\theta}}|\boldsymbol{\theta})$$
 (31)

where

$$\sigma(l, j|l', j'|\theta) = \frac{\pi}{k^2} (2l+1) T_t(E) \sum_{J} \frac{A_J(l, j|l', j'|\theta)}{1 + \sum_{q, q, J} T_q(E_q') / T_1'(E')}, \quad (32)$$

and is the cross section for production of neutrons of energy E' of angular momentum l', channel spin j', moving in a direction θ . The r index refers to possible channel spins, p to possible final neutron angular momenta, E'_t to final neutron energies. J is the total angular momentum of the compound nucleus state. The prime on the summation indicates that we omit the term of the final field. cates that we omit the term referring to the final neutron E', l', j' we are considering. As we shall see the denominator of eq (32) is essentially the branching ratio of the specific neutron transition under consideration versus all other possibilities. If we immediately specialize to the case of compound clastic scattering, (E=E', l=l', j=j'), consider spin zero nuclei only $(j=j'=\frac{1}{2}, i=0, \text{ and } J=l\pm\frac{1}{2})$, and T_1 's as defined in eq (29), the angular distribution for the lth partial wave of compound elastically scattered neutrons becomes:

$$\left(\frac{d\sigma}{d\Omega}\right)_{l_{CE}} = \frac{\pi}{2k^{2}} \left\{ \frac{(l+1)T_{l}^{+}(E)}{1 + \sum_{p,q,r} T_{p}^{+}(E_{q}^{+})/T_{l}^{+}(E)} A_{l+1} \left(l_{r}\frac{1}{2} \left| l_{r}, \frac{1}{2} \right| \theta\right) + \frac{lT_{l}^{-}(E)}{1 + \sum_{p,q,r} T_{p}^{+}(E_{q}^{+})/T_{l}^{-}(E)} A_{l-1} \left(l_{r}, \frac{1}{2} \left| l_{r}, \frac{1}{2} \right| \theta\right) \right\} \cdot (33)$$

The A-functions that occur in eq (33) are easily expressed in terms of Z-coefficients used by Blatt and Biedenharn (1952) and tabulated by Biedenharn (1953):

$$A_{I}(l,j|l,j|\theta) = \frac{1}{4\pi(2l+1)} \sum_{L} [Z(lJlJ;jL)]^{2} P_{L}(\cos\theta).$$
(34)

The question of phases does not enter since the Z-coefficient appears only when squared. Note that these results appear naturally in a Legendre series expansion which may be easily combined with the Legendre coefficient expansion as determined by the computer for the shape elastic scattering. Equations (33) and (34) are used to calculate the region of discrete states of the target nucleus (3.35 to 5 Mev). A correction to the branching ratio appearing in eq (33) is applied to allow for experimentally observed reaction cross sections. From 5 to 5.7 Mev, the residual nucleus is considered as statistical, and the compound elastic scattering is isotropic.

2.4. Legendre Coefficient Analysis of the Elastic Scattering

The elastic scattering angular distribution is represented in the following way:

$$\frac{d\sigma}{d\Omega}(E,\theta) = \frac{\sigma_{\text{total elastic}}}{4\pi} \sum_{l} (2l+1)S_{l}(E)P_{l}(\cos\theta) \quad (35)$$

where $S_0(E) = 1$.

The differential cross section as obtained from eq (24) appears as a sum of the products of two series:

$$\begin{split} \frac{d\sigma}{d\Omega} &= \sum_{l} A_{l} P_{l}(\cos\theta) \sum_{m} A_{m} P_{m}(\cos\theta) \\ &+ \sum_{l} B_{l} P_{l}^{1}(\cos\theta) \sum_{m} B_{m} P_{m}^{1}(\cos\theta). \quad (36) \end{split}$$

The first term in eq (36) may be represented by a single series of Legendre coefficients

$$\frac{d\sigma}{d\Omega} = \sum_{k} a_{k} P_{k}(\cos\theta), \qquad (37)$$

where a_t is given by

$$a_{k} = \sum_{l=0} \sum_{m=0} A_{l} B_{m} \frac{C_{\frac{1}{2}(l-m+k)} C_{\frac{1}{2}(l+m-k)} C_{\frac{1}{2}(m-l+k)}}{C_{\frac{1}{2}(l+m+k)}} \times \frac{2k+1}{l+m+k+1}, \quad (38)$$

where $C_i = \frac{1.3.5 \dots (2j-1)}{j!}; l, m$ are positive integers; (l+m+k) is even; and $|l-m| \le k \le l+m$, that is, the three vectors satisfy the "triangle condition" [Whittaker and Watson, 1958].

The product of the two series in $P_i(\cos \theta)$ can be reduced to product of two series in $P_i(\cos \theta)$ which can then be solved by eq (38). First we express the $P_i(\cos \theta)$'s in terms of polynomial expansions in $P_i(\cos \theta)$ [see Morse and Feshbach, 1953]:

$$P_{i}^{i}(\cos\theta) = \frac{l(l+1)}{(2l+1)\sin\theta} [P_{l-1}(\cos\theta) - P_{i+1}(\cos\theta)]$$
(39)

$$\begin{split} P_{m}^{1}(\cos\theta) = & \sin\theta [(2m-1)P_{m-1}(\cos\theta) \\ & + (2m-5)P_{m-2}(\cos\theta) \\ & + (2m-9)P_{m-5}(\cos\theta) + \dots] \quad (40) \end{split}$$

Any product term $P_1^1(\cos\theta)P_n^1(\cos\theta)$ resulting from the series product in eqs (36) may be expressed in terms of a product of expressions from eqs (39) and (40). Note that in the product $\sin\theta$ cancels out, leaving only terms in Legendre polynomials. Relations (38 to 40) were programed for the computer so that a Legendre coefficient analysis of the form of eq (35) could be directly obtained from the calculated phase shifts.

The calculation could equally well be done through use of vector-coupling coefficients [Edmonds, 1957]. It is expected that the problem for the computer would be about the same either way. The C₁ coefficients used here are closely related to the Clebsch-Gordan coefficient (ab00|abc0) as given in eq (5) of Blatt, Biedenham, and Rose [1952].

Choice of Optical Model Parameters and Comparison With Experiment

Calcium is composed of 96.97 percent Ca¹⁰ with 2.06 percent of Ca⁴¹, and smaller amounts of Ca⁴², Ca⁴³, Ca⁴³, and Ca⁴⁶. In this calculation it is considered as pure Ca⁴⁰ except that a slightly larger value of R_0 is used to approximate the effect of the other isotopes.

In the initial attempts to fit calcium neutron cross section data, the model of Bjorklund and Fernbach [1958] was used. The real potential is as described by eq (7), and the imaginary potential is a Gaussian absorption located at the surface:

$$W = W_r \exp\left[-\left(\frac{r - R_0}{b}\right)\right]^t. \tag{41}$$

This model, which has been quite successful in fitting neutron elastic scattering data at 4.1, 7, and 14 Mey, involves six parameters: R_0 , V_c , α , a, W_s , and b. In attempting to fit this data, R_0 was held constant at 1.25 $A^{1/3}$ fermis, b at 0.980 fermis, α at 35. The average atomic weight was used for A. The other three parameters were varied. A problem of the optical model is the large number of arbitrary parameters. In an attempt to reduce the number of parameters the width of the surface absorption, b, was eliminated as an independent parameter and derivative surface absorption used instead as given in eq (8). Somewhat surprisingly the agreement with the experimental data was considerably improved at 14.6 Mey, and was equally good at the energies of 2 Mey and below where data existed which could be directly compared with optical model predictions using the fluctuation cross section. The improved agreement at 14.6 Mev may be stated in another way; namely, the value of b(0.980 fermis) is too small at this energy, and a thicker shell of surface absorption of neutrons should be used. This is given automatically by the use of a derivative surface absorption.

Using the derivative surface absorption model, R_0 was held constant at 1.25A 1/2 fermis, the value indicated by the work of Bjorklund and Fernbach, and also by the optical model analyses of proton polarization reported by Gursky and Stewart [1961]. Actually the parameters V_c and R_o act very much like a single parameter V_cR_o , where n is equal to 2 at low energies and increases slightly with energy. Our choice is to hold Ro fixed and vary V. The strength of the spin-orbit coupling, α , was also held at the value of 35 used by Bjorklund and Fernbach because it was felt that changes or improvements in this value should come from the analysis of polarization data to which α is more sensitive, rather than angular distribution data which is considered here. Three parameters were allowed to vary, V_{ϵ} , W_{ϵ} , and a. Although a could have been held fixed, independent of energy, at a value of about 0.580 fermis to obtain fairly good fits to the experimental data everywhere, it was found that better fits were obtained if a was taken as 0.600 fermis at 14.6 Mey and at 0.550 fermis below 2 Mev. Smooth curves drawn through the data were used to obtain parameters for the optical model calculations, even though local variations sometimes gave better fits (see fig. 2). This apparent jumping around of the experimental data is due at the low energies to the presence of resonances in the cross section, which the optical model averages over,

It should also be mentioned that a calculation which predicts the energy variation of the parameters of the optical model by use of a nonlocal potential has been made by Perey and Buck [1961]. The predictions of Perey and Buck have not been used here since it seemed unlikely that they would

improve the cross section data.

Experimental data used for the parameter determination at 14.6 Mev were taken from Cross and Jarvis [1960]; below 2 Mev, the data of Seagrave, Cranberg, and Simmons [1958] and Lane, Langs-

dorf, Monahan, and Elwyn [1960] as collected by Howerton [1961] were used. Comparison of the calculation to experimental data is shown in figures. 3 through 12. Comparison is also made to data at

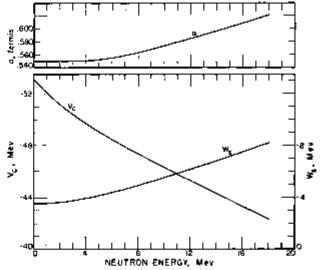
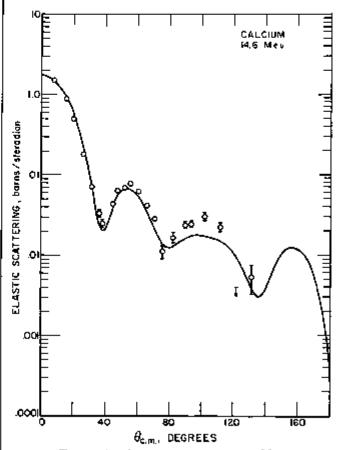


FIGURE 2. Optical model parameters versus energy as adopted for the calculation.



Flaves 3. Etastic scattering at 14.6 Mev.

Experimental data are those of Cross and Jarvis [1960]. The corves in this and succeeding figures are from this calculation using the optical model parameters of figure 2

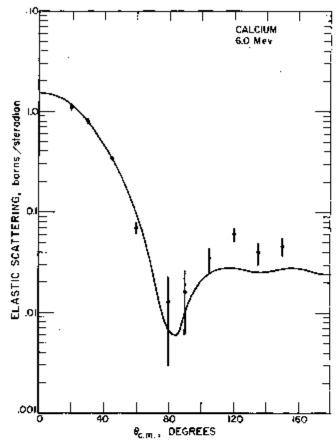


FIGURE 4. Blastic scattering at 6.0 Mev. Experimental data are from Sesgrave, Cranberg, and Simmons [1988].

4.1 Mev of Vincent, Morgan, and Prud'homme [1960] and to an angular distribution of Seagrave, Cranberg, and Simmons [1958] at 6.0 Mev. Neither of these distributions was used to obtain the optical model fit because the Hauser-Feshbach hand calculation involved made parameter fitting quite difficult (it later turned out that at 6.0 Mev the compound elastic scattering could be neglected). Nevertheless the agreement between calculation and experiment is about the same here as at the other energies. We may therefore be reasonably confident that the calculation predicts the cross sections quite well where they have not been measured.

It would not be possible for these calculations to agree with both the Seagrave et al. and the Lane et al. experimental measurements, since these disagree with each other. In general the angular distributions of Lane et al. are more isotropic, while the distributions of Seagrave et al. have a larger cross section in the forward direction. Somewhat more weight was given to the Seagrave et al. experiment, since the geometry appears to be somewhat cleaner and less subject to multiple scattering effects which would tend to make the distributions too isotropic.

This optical model underestimates the magnitude of the non-elastic (or compound nucleus formation) cross section at 14.5 Mev. The calculation gives

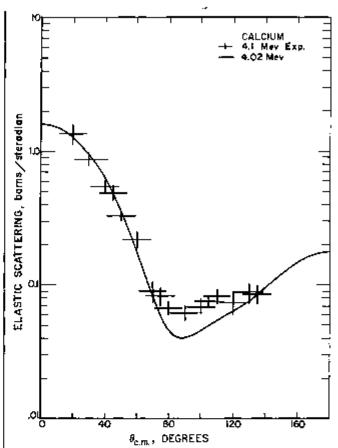


FIGURE 5. Etastic scattering at 4.02 Mev.

The calculation is compared to the 4.1 Mev experimental data of Vincent, Morgan, and Producence [1969].

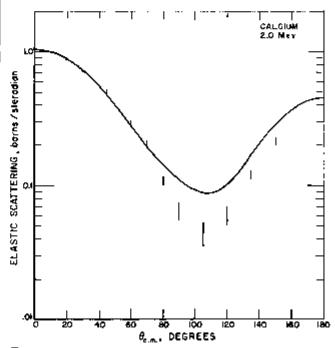


FIGURE 6. Elastic scattering at 2.0 Mev.

Experimental data are from Seagrave, Cranberg, and Simmons (1968).

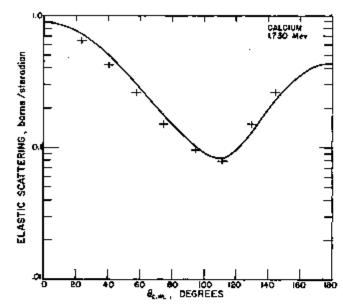


Figure 7. Elastic scattering at 1.730 Mev.

Experimental data are from Lone, Lone, Laugsdorf, Monglum, and Elwyn
1860].

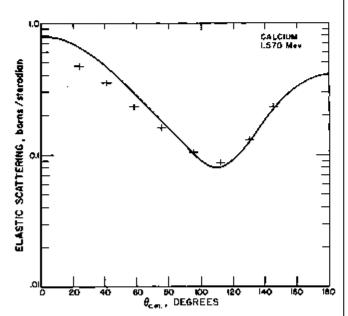


FIGURE 8. Elastic scattering at 1.570 Mev.
Experimental data are from Lane, Langedorf, Monaban, and Elwyn [1988].

1.227 barns at 14.6 MeV, whereas the experimental measurement at 14.5 MeV of Flerov and Talyzin [1956] gives 1.36 ± 0.02 barns. This leads to a corresponding error in the total cross section, but does not affect the elastic cross section values. The total elastic cross section at 14.6 MeV is 0.803 barns, in agreement with the experimental value of 0.82 ± 0.07 barns of Cross and Jarvis.

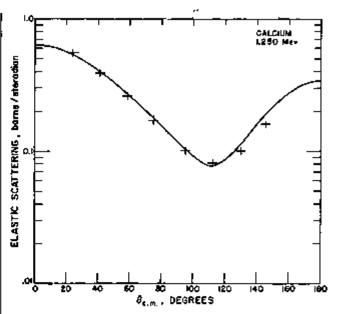


Figure 9. Elastic scattering at 1.250 Mev. Experimental data are from Lane, Langedorf, Monahan, and Elwyn [1960].

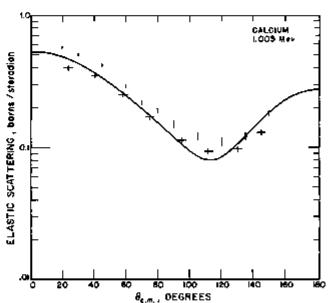


FIGURE 10. Elastic scattering at 1.005 Mev.

Experimental data are from Lane, Langsdorf, Monahan, and Elwyn [1960] at 1.01 ± 0.03 Mev (present) and Irom Sesgrave, Cramberg, and Simmons [1938] at 1.0 Mev (vertical lines).

4. Results of the Calculation

The calculated angular distributions for total clastic scattering are given in table 1 and the Legendre coefficient expansions are given in table 2.

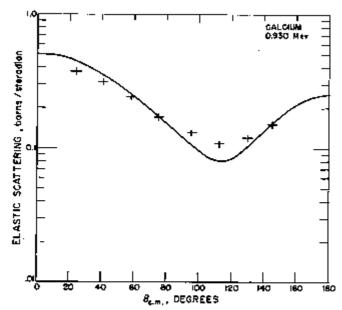


FIGURE 11. Elastic scattering at 0.930 Mev.
Experimental data are from Lane, Langdorf, Monahan, and Elwyn [1906].

Table 1. Angular distributions of neutron elastic scattering for calcium (barns/steradian)

| 649 0.0 10.0 18.0 20.0 | 18,000 Mer 2,2740 2,1104 1,6774 1,1189 0,5980 | 17. 100 Mey 2 1727 2.0223 1. 6223 1. 1011 0. 6068 | 16. 300 Mev 1. 9627 1. 6512 1. 4996 | 15.600 Mev 1.8449 1.7277 | 14, 750 Mev L 7511 I, 6449 | 14, 000 MeV | 13. 300 Mev 1. 5969 |
|--|---|---|---|-----------------------------------|-------------------------------------|----------------|---------------------------|
| 0. 5. 0 10. 0 15. 0 20. 0 25. 0 | 2, 1104 1, 6774 1, 1189 0, 5980 | 2. 0223 1. 6223 1. 1011 | 1. 8512 1. 4995 | 1.7277 | | | 1 5989 |
| 0. 5. 0 10. 0 15. 0 20. 0 25. 0 | 2, 1104 1, 6774 1, 1189 0, 5980 | 2. 0223 1. 6223 1. 1011 | 1. 8512 1. 4995 | 1.7277 | | | 1 5000 |
| 8. 0 10. 0 18. 0 20. 0 20. 0 | 2, 1104 1, 6774 1, 1189 0, 5980 | 2. 0223 1. 6223 1. 1011 | 1. 8512 1. 4995 | 1.7277 | | | |
| 10. 0 15. 0 20. 0 26. 0 30. 0 | 1. 6774 1. 1189 0. 5980 | 1. 8223 1. 1011 | 1.4996 | | | 1. 5857 [| 1.5013 |
| 18. 0 20. 0 20. 0 30. 0 | 1. 1189 0. 5980 | L. tota | | | 1.3364 | 1. 3234 | 1.2885 |
| 20.0 4 25.0 30.0 | 0. 5980 | | | 1.4131 | | | |
| 28. U 30. O j | I | | | 0.9947 | 0.9740 | D. 9678 | 0.9495 |
| 30.0 | 9000 | 10.0000 | 0.5883 | . 5942 | . 5906 | . 8074 | . 6203 |
| 30.0 | | .2467 | .2544 | . 2684 | . 2884 | .3147 | .3451 |
| | .0438 | .0339 | .0577 | .0637 | 1029 | | . 1385 |
| 35.0 | 0031 | .0027 | .0084 | .086 | .0261 | 0384 | .0814 |
| 40.0 | .0340 | | .0232 | .0212 | . 0206 | 0212 | .0510 |
| | .0755 | . 0270 . 0837 | . 0482 | .0507 | .0437 | .0386 | .0334 |
| 45.0 | -0340 | - 128657 | . UKWKZ | . 10007 | . 19437 | .0306 | . 0854 |
| 50.0 | .0914 | . 0847 | . 0767 | .0712 | . 0889 | .0545 | .0479 |
| 55.0 | .0792 | .0772 | 0743 | 0712 | 0880 | .0600 | .0533 |
| 60.0 | 0327 | .0112 | 0444 | .0553 | . 0511 | 0323 | .0484 |
| 65.0 | .0251 | . 0302 | . 0330 1 | . 0350 | .0588 | .0377 | . 0371 |
| 70.0 | .0142 | . 0102 | . 017.1 | .0197 | .0220 | .0237 | .0251 |
| 241.0 | . 0142 | . Dtaz | ו הנדום. | . 4184 | .0220 | ا بعضاد | . 0231 |
| 76.0 | .0112 | . 0106 | . OLL7 İ | .0123 | .0142 | .0947 | . 0182 |
| 80.0 | 0141 | .0127 | .0120 | 0128 | 0127 | .0113 | ÜİİB |
| 80.0 | .0174 | .0181 | .0181 | 0154 | .0148 | .0117 | บาน |
| 910 | .0178 | .0173 | .0179 | .0174 | .0164 | 0189 | 0130 |
| 92.0 | .0132 | .0138 | .0170 | 0175 | .0175 | .0162 | 0182 |
| | | | | | .0174 | | 1 00000 |
| 100.0 | . 0110 | . 0121 | . 0143 | 0160 | .0174 | .0179 | . 0194 |
| 103.0 | .0072 | . 0088 | .0113 | 0139 | .0108 | .0184 | .0217 |
| 110.0 | .0049 | . 0061 | .0068 | .0119 | .0152 | . 0175 | 0219 |
| 114.0 | .0040 | . D048 | .0072 | .0000 | .0130 | .0150 | .0196 |
| 120.0 | .0039 | .0042 | . 0039 | 0079 | 0100 | ,0113 | . 0150 |
| | | | | | | | |
| 123.0 | . 0038 | . 0038 | .0047 | .0057 | .0067 | - 0071 | . 0098 |
| 120.0 | . 0033 | . 0032 | 0036 | .0038 | .0041 | .0089 | . 0047 |
| 124.0 | .0028 | . 0028 | . 0031 | I HINEL | .0080 | .0027 | . 0028 |
| 140.0 | .0026 | . 0029 | . 0035 | - OUGH I | .0041 | .0039 | .0048 |
| 145.0 | .0029 | . 0035 | .0048 | .0050 | .0089 | -0071 | .0085 |
| | | | | | | | |
| 150.0 | .0033 | .0044 | . 0064 | 0083 | .0101 | .0105 | . 0181 |
| 155.0 | .0042 | . 0032 | . 0076 | .0099 | .0121 | .0126 | .0101 |
| 160.0 | .0048 | .0032 | 0075 | .0097 | .0117 | -0123 | .0167 |
| 165.0 | .0049 | .0048 | .0063 | .40077 | . 0090 | .0093 | . 0120 |
| 170.0 | .0045 | .0039 | . 0043 | .0047 | .0051 | 0051 | . 0067 |
| 175.0 | .0040 | .0030 | .0028 | .0021 | .0017 | .0015 | . 0020 |
| 180.0 | .0028 | .0028 | .0012 | 0010 | .0004 | .0000 | . 0001 |

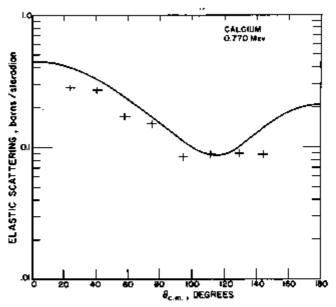


FIGURE 12. Elastic scattering at 0.770 Mev.
Experimental data are from Lang, Langsdorf, Modulana, and Elwyn [1066].

Table 1. Angular distributions of neutron elastic scattering for calcium (harns/steradian)—Continued

| | | | | | | <u> </u> | |
|--------------|---------------|---------------------|----------------|----------------|----------------|-----------------|-----------------------------|
| Anglo | 12,700 Mev | 12, 100 Mev | 11. 500 Mev | 10, 900 Mev | 10. 400 Mev | 9. 890 Mev | 9,410 Mev |
| 409 | | <u> </u> | | | | | |
| Q | 1. 5352 | 1, 4555 | 1. 4105 | 1.3773 | 1.8298 | 1.8199 | 1.8476 |
| 5.0 | 1. 4571 | 1.3852 | 1.8492 | 1.3219 | 1.2916 | 1.2766 | 1.8061 |
| 10.0 | 2, 2484 | 1.1979 | 1.1794 | 1. 1679 | 1.1470 | 1. 16[1 | 1. 1891 |
| 25.0 20.0 | 0.9480 | 0.9857 | 0.19393 | 0.9478 | 0.9521 7521 | 0.9892 .7809 | 1. 01 6 5 0. 2159 |
| 20.0 | . 6382 | . 6555 | .0781 | .7089 | 11921 | . 1999 | 0.2109 |
| 25.0 | .8726 | .4078 | . 4410 | .4768 | . 5212 | .6671 | . 6152 |
| 30.0 | . 1849 | . 2238 | . 2577 | .2945 | .8445 | . 3815 | . 4870 |
| 85.0 | .0792 | . 1109 | . 1879 | . 1984 | .2143 | . 2470 | , 2046 |
| 40.0 | .0882 | .0578 | . 0789 | .0947 | . 1302 | 1658 | . 1016 |
| 45.0 | . 0345 | .0418 | .0499 | .0699 | .0832 | . 0997 | . 1240 |
| 60.0 | .0484 | .0428 | .0420 | .0480 | .0604 | . 0695 | . 0830 |
| 55.0 | .0491 | 0450 | 0145 | 0448 | .0497 | 0685 | .0588 |
| 80.0 | .0466 | .0441 | . 0428 | .0417 | . 0425 | 0431 | 0433 |
| 65.0 | . 0575 | . 0808 | - 0362 | . 0852 | - 0346 | .0334 | .0312 |
| 70.0 | . 0259 | . 0268 | 0254 | .0256 | - 0247 | . 0282 | . 0205 |
| 76.0 | . 0162 | .0171 | .0164 | .0155 | .0148 | .0134 | .0113 |
| 80.0 | .0105 | .0206 | .0091 | ,0079 | .0078 | 0063 | .0051 |
| 86.0 | 0000 | . 0079 | . 006j | .0046 | .0042 | 0005 | .0022 |
| 90.0 | . 0108 | .0096 | .0378 | .0068 | -0062 | ,0057 | .00% |
| 95.0 | . 0148 | .0144 | -0131 | .0119 | -0123 | . 0117 | .0121 |
| 100.0 | .0193 | . 0206 | .0198 | .0180 | .0202 | . (1193 | .0198 |
| 106.0 | . 0226 | .0255 | . 0254 | 0247 | .0289 | .0267 | . 0257 |
| 110.0 | . ((233 | 0274 | 0276 | .0271 | 0228 | .0286 | .0284 |
| 115.0 | . 0209 | . 0252 | . 025) | . 0252 | .0281 | 0270 | .0239 |
| 120.0 | - 0148 | . 0t04 | . 0197 | .0107 | .0223 | 8150 | . 0221 |
| 125.0 | . 0097 | . 0121 | .0124 | .0127 | .0149 | .0151 | .0158 |
| 130.0 | .0047 | .0049 | .0062 | . 0069 | .0088 | . 0096 | .0108 |
| 135.0 | .0027 | . 0032 | . 0033 | .0043 | .0037 | . 0087 | .0081 |
| 140.0 | . 0042 | .0048 | .0049 | .0063 | .0000 | . 0076 | .0090 |
| 145.0 | . 0083 | -0006 | .0094 | -0003 | .0109 | .0111 | .0122 |
| 150.0 | . 0130 | . 0162 | .0146 | .0139 | .0158 | . 0152 | . 0159 |
| 155. Ů | .0139 | . 0188 | .0179 | .0169 | .0190 | . 0178 | .0182 |
| 180.0 | .0156 | .0186 | .0178 | 0168 | .0168 | . 0176 | .0179 |
| 165.0 | .0121 | . 01 0 0 | .0143 | . 0137 | .0154 | . 0145 | .DI49 |
| 170.0 | .0070 | . 00 9 6 | . 0069 | .0000 | .0108 | , 0100 | . DID6 |
| 175.0 | . 0025 | . 0034 | . 0042 | .0048 | .0048 | .0081 | .0089 |
| 180. ŏ | .0007 | .0013 | .0023 | .0032 | .0040 | .0048 | . 0055 |
| | | | | ' | | | |

Table 1. Angular distributions of neutron elastic scattering | for calcium (barns/steradian)—Continued

8,930 Mey. 7.700 Mev. Angle 8.610 Mey B.100 Mey 6.662 Mev. Mev. Mey, deg O 1. 4620 1. 4220 1. 2426 1. 2431 1. 0491 1. 4828 1. 4532 1. 3687 . 2131 4324 1, 3728 5.0 10.0 15.0 1. **6010** 1. **3103** 1. 1722 31.00 1, 3211 1, 2209 L 3389 L 2422 1, 3795 1, 2867 2030 1. 2386 1. 0766 1,0692 1.0982 0.9205 1. T457 20. Ď 0.8472 0. 9741 1 0046 25. 0 30. 0 35. 0 40. 0 45. 0 . 7356 . 5676 . 4087 . 2861 . 1939 0. 8704 . **693**0 . 5294 0.8990 .7211 .3334 4413 .7014 0.9231 . 473fl . 327fl 5265 3775 . 614 6457 4953 . 4565 3257 .2503 .1746 . 4106 . 2910 9189 3500 . \$882 . 2731 1429 2937 2428 50, 0 55, 9 60, 0 65, 0 70, 0, . 0946 . 0646 . 0456 . 0308 1156 1784 . 1485 1817 1839 1972 . 0763 0500 . 0835 . 0831 . 0952 . 0585 1034 1270 0719 0768 .0397 .0196 . 0193 .DIX3 0179 .0175 0120 0211 75. 0 80. 0 86. 0 90. 0 95. 0 0109 **008**5 . COTAC .0078 0029 mei 0001 0045 .0039 .0032 .0065 .0036 .0032 .0065 0035 0039 0046 0091 . 0034 .0037 0038 .0048 .0087 0058 0118 0125 0123 0135 0132 0145 0142 100.0 6199 ()102 . 0196 . 0248 . 0264 . 0257 . 0190 . OLS6 0201 0197 100.0 105.0 110.0 115.0 120.0 .6247 .6271 .0260 0245 . 17236 0247 0239 0270 0259 0251 0255 0267 0281 0051 0060 0010 125, 0 180, 0 186, 0 140, 0 145, 0 .0161 . 0174 . 0191 0199 0219 .0132 .0112 .0116 .0137 .0144 .0126 .0129 .0148 .0161 .0146 .0150 .0165 OHIA 0174 . 01189 .0213 . 0094 0182 0185 .0207 . 01109 .0212 . D127 . Da 77 0204 .0222 150. 0 155. 0 160. 0 165. 0 170. 0 . 0162 . 0175 . 0180 **B157** .0181 0189 0218 .0231 .0187 .0178 .0155 .0125 0192 0182 0218 0232 D174 0179 0145 0140 0109 .0168 .0141 .0143 .0180 .0188 0188 0103 .0204 .0183 .0103 175. 0 .0079 0083 . 0101 . 00 11 .0165 . 00 48 180. Č .0058 .0067 0073 .0091 .0108 .0135 .0159 Angle 8.500 Mev. 8.000 6.700 5.430 Mev. 5,160 Mev. 4,910 Mev. 4.870 Mov. Mev. Mev. ₫⊗ 0, 5, 0 0, 2 1. 5678 1. 5411 1. 4651 1. 3464 1. 1956 1,5719 1,5464 1,4728 1,8568 1,2087 1.5277 1.5109 1.4335 1.3128 1, 5018 1, 4726 I. 6092 I. 6837 1.60**23** 1.5786 1.5259 1, 4990 1, 4199 1, 4199 1, 2988 1. \$897 1. 2617 1. 1018 10.0 15.0 0006 3036 M64 20.0 1. 1409 I. 1604 1. 2453 1.2483 0.9254 .7473 .5799 .4521 .3086 25.0 30.0 85.0 40.0 0.9891 .7910 .6219 0. 9894 . 8134 1. 0255 0. 8489 . 6774 1.0414 0.9669 .6666 .5266 1, 0922 0, 9097 , 7387 , 5792 0770 0.9006 6439 APORT 4900 6471 45.0 3935 4019 4264 . 2103 2343 2497 . 2704 . 2872 . 3181 55.0 80.0 85.0 . 9363 . 0828 . 0463 . 0231 . 1813 . 1149 . 0689 . 0389 . In31 .0025 1854 1981 . 1981 9112 . 2218 . 1276 . 0791 . 0474 1481 0394 Deute: 0477 70. O 0202 0316 0.89 0038 75. 0 90. 0 85. 0 0102 .0117 DIRO 0212 .0220 .0049 .00% .00% 0083 0089 0120 .0206 .0191 0247 0227 0282 03.72 90. 0 95. 0 .0096 .0138 .0099) 01220218 0250 0.269 0142 .0173 .0225 0306 OYLY .0266 100.0 0190 0207 0223 0971 0217 0344 0352 105. D 110. O .0231 .0256 0340 .0288 .0261 .0262 .0388 0395 10044 . **026**0 .0307 0389 0412 0447 . 0458 . 0488 120.0 0277 125, 0 130, 0 135, 0 140, 0 145, 0 0428 0435 0446 0460 .0303 .0302 .0489 .0515 4939 0267 nasa 0515 . 0383 . 0388 0250 0228 0227 0206 0204 0551 0587 0281 0378 .0853 .0477 02420270 0322 0649 .0718 150, 0 155, 0 160, 0 163, 0 0251 0252 0244 0229 0339 0337 0336 0329 .0402 .0411 .0414 .0411 .0406 . 0494 . 0606 . 0516 . 0519 0707 0767 0791 0864 0984 0994 0278 0280 0278 0280 0280 0824 0872 0910 170. O 0210 0310 .0318 . 1042 .0401 .0299 175.0 .0198 0241 0237 0933 . 0190 .0316 D941 J80. C .0306 .1092

Table I. Angular distributions of neutron elastic scattering for calcium (barns/steradian)—Continued

| Angle | 4.440 | 4.230 | | 1.020 3.620 3.640 | | | 5.260 | |
|---|---|--|---|---|--|--|--|--|
| | Mer | Mev | Mov | Mea | Mev | 3.480 Mer | Mev | |
| 5.0 10.0 14.0 20.0 | 1, 7219 1, 6938 1, 6116 1, 4632 1, 3100 | 1. 6196 1. 5889 1. 5197 1. 4109 1. 2710 | L 3696 L 3763 L 3093 J. 4084 J. 2672 | 1. 8072 1. 5836 1. 5150 1. 4077 1. 2719 | L 3998 L 3787 L 3208 1, 2296 1, 1132 | 1,5570 1,6360 1,4746 1,3778 1,2522 | 1. 570x 1. 549 1. 4894 1. 894 1. 271 | |
| 25.0 | 1. 1321 | 1. 1107 | 1.1109 | 1. 1161 | 0. 9709 | 1, 1074 | 1, 1295 | |
| 20.0 | 0. 9386 | 0. 9408 | 0.9449 | 0. 9529 | .8394 | 0, 9525 | 0, 9751 | |
| 35.0 | . 7455 | . 7719 | .7794 | . 7907 | .7005 | , 7966 | , 8204 | |
| 40.0 | . 5896 | . 6126 | .6229 | . 6370 | .5706 | , 0475 | , 6724 | |
| 45.0 | . 4170 | . 4698 | .4816 | . 4971 | .4559 | , 5115 | , 5370 | |
| 50.0 | . 2923 | .3475 | .3602 | . 3749 | .3592 | . 9927 | .4194 | |
| 55.0 | . 1972 | .2477 | .9604 | . 2787 | .2824 | . 2988 | .2294 | |
| 60.0 | . 1304 | .1703 | .1623 | . 1915 | .2250 | . 2148 | .2421 | |
| 65.0 | . 0684 | .1138 | .1247 | . 1319 | .1854 | . 1552 | .1825 | |
| 70.0 | . 0665 | .0754 | .0650 | . 0900 | .1607 | . 1129 | .1396 | |
| 75.0 90.0 85.0 90.0 95.0 | . 0589 . 0600 . 0646 . 0691 . 0702 | .0519 .0598 .0352 .0358 .0590 | . 0800 . 0464 . 0408 . 0404 . 0428 | .0651 .0524 .0479 .0476 .0491 | .1475 .3421 .1409 .1410 .1401 | . 0850 . 0085 . 0002 . 0574 . 0579 | . 1091 . 0017 . 0377 . 0776 | |
| 100.0 105.0 110.0 115.0 120.0 | . 0658 . 0500 . 0863 . 0261 | .0432 .0475 .0514 .0552 .0591 | .0684 .0505 .0587 .0686 | .0511 .0534 .0567 .0816 .0884 | . 1885 . 1801 . 1204 . 1088 . 0948 | ,0601 ,0634 ,0675 ,0725 ,0791 | .0780 .0812 .0834 .0915 .0990 | |
| 125.0 | . 0200 | .0637 | . 0694 | .0769 | . 0606 | .0977 | . 1096 | |
| 130.0 | . 0201 | .0603 | . 0765 | .0965 | . 0077 | .0987 | . 1256 | |
| 135.0 | . 0277 | .0762 | . 0662 | .0968 | . 0662 | .1126 | . 1425 | |
| 140.0 | . 0430 | .0846 | . 0965 | .1079 | . 0474 | .1293 | . 1647 | |
| 145.0 | . 0654 | .0942 | . 1076 | .1189 | . 0417 | .1485 | . 1907 | |
| 150.0 | .0033 | .1047 | , 1206 | . 1335 | . 0392 | . 1698 | . 2191 | |
| 155.0 | .1243 | .1156 | , 1344 | . 1495 | . 0397 | . 1915 | . 2484 | |
| 160.0 | .1555 | .1261 | , 1473 | . 1662 | . 0425 | . 2128 | . 2765 | |
| 166.0 | .1839 | .1364 | , 1682 | . 1834 | . 0464 | . 2319 | . 3013 | |
| 170.0 | .2005 | .1428 | , 1680 | . 1982 | . 0505 | . 2471 | . 3207 | |
| 175. § | . 2212 | . 1473 | . 1747 | . 2083 | . 0534 | . 2568 | . 8331 | |
| 180. û | . 2262 | . 1491 | . 1788 | . 2121 | . 0545 | . 2602 | . 8374 | |
| Angle | 2.970 | 2.890 | 2.440 | 2.210 | 2.000 | 1.810 | 1.620 | |
| | Mev | Mev | Mey | Mev | Mey | Mev | May | |
| drg 0. 5.0 10.0 15.0 20.0 | 1. 4990 1. 4793 1. 4218 1. 3311 1. 2143 | 1, \$767 1, \$60\$ 1, \$12\$ 1, 2581 1, 1569 | 1. 2546 1. 2405 1. 1991 1. 1332 1. 0473 | 1. 1456 1. 1854 1. 0975 1. 0403 0. 9650 | 1.0433 1.0527 1.0017 0.9523 .8878 | 0.9909 .9221 .8963 .8552 .8013 | 0. 8244 - 8177 - 7962 - 7625 - 7185 | |
| 25.0 | 1, 0797 | 1.0211 | 0.9466 | . 8779 | .8111 | . 7378 | - 6665 | |
| 30.0 | 0, 9364 | 0.8957 | .8374 | . 7822 | .7278 | . 6681 | - 6685 | |
| 35.0 | . 7927 | .7079 | .7258 | . 6838 | .6417 | . 6666 | - 5476 | |
| 40.0 | . 6556 | .6440 | .6160 | . 5878 | .8469 | . 6241 | - 4865 | |
| 45.0 | . 5311 | .5290 | .5138 | . 4964 | .4767 | . 4554 | - 4286 | |
| 50.0 | . 4219 | .4269 | . 4229 | .4142 | . 4138 | 3019 | . 373) | |
| 55.0 | . 3296 | .3366 | . 3428 | .8425 | . 3391 | 3349 | . 323; | |
| 60.0 | . 2550 | .2082 | . 2764 | .2818 | . 2839 | 2851 | . 278; | |
| 65.0 | . 1962 | .2119 | . 2280 | .2821 | . 2380 | 2424 | . 240; | |
| 70.0 | . 1520 | .1094 | . 1814 | .1924 | . 2005 | 2065 | . 207] | |
| 75.0 | . 1201 | . 1887 | .1800 | . 1614 | . 1704 | .1767 | . 178' | |
| 80.0 | . 0668 | . 1175 | .1268 | . 1376 | . 1465 | .1520 | . 154 | |
| 85.0 | . 0656 | . 1036 | .1102 | . 1196 | . 1276 | .1315 | . 133' | |
| 90.0 | . 0795 | . 0949 | .0986 | . 1061 | . 1127 | .1146 | . 116' | |
| 95.0 | . 0782 | . 0900 | .0908 | . 0902 | . 1013 | .1015 | . 101' | |
| 100, 0 | .0903 | .0879 | .0962 | . 0696 | .0933 | .0916 | . 090 | |
| 105, 0 | .0848 | .0882 | .0846 | . 0664 | .0889 | .0856 | . 063 | |
| 110, 0 | .0908 | .0910 | .0863 | . 0670 | .0685 | .0841 | . 061 | |
| 115, 0 | .0981 | .0968 | .0917 | . 0920 | .0930 | .0878 | . 063 | |
| 120, 0 | .1008 | .1063 | .1016 | . 1021 | .1032 | .0974 | . 062 | |
| 125.0 130.0 | . 1170 . 1816 . 1496 . 1727 . 2006 | 9202 1291 1632 1922 2252 | . 1168 . 1373 . 1640 . 1937 . 2213 | . 1181 . 1403 . 1696 . 2025 . 2407 | .1196 .1428 .1729 .2071 .2466 | . 1138 . 1368 . 1846 . 1986 . 2367 | . 1073 . 129 . 1573 . 190 . 227 | |
| 140.0 145.0 | | . 2807 | .2698 | . 2814 . 3223 | . 2885 . 3905 | . 2770 . 3172 | . 266 . 304 | |
| 135.0 140.0 | . 2326 . 2671 . 8016 . 3329 . 3480 | . 2967 . 3309 . 3608 . 3641 | . 2084 . 2448 . 2765 . 4011 | . 3608 . 3943 . 4202 | . 3899 . 4041 . 4304 | .3550 .3877 .4130 | 340 370 394 406 | |

Table 1. Angular distribution of neutron elasti-for calcium (barne/steradian)—Continued

0, \$193 . \$172 . \$111 . \$013 . 2883

. 2726 . 2550 . 2560 . 2165 . 1989

. 1778 . 1646 . 1424 . 1284 . 1117

. 0083 . 0801 . 0752 . 0858 . 0575

1.340 Mev

0. 6742 . 6691 . 6541 . 6301 . 5982

. 5802 . 5178 . 4780 . 4275 . 3829

. 3404 . 3007 . 2546 . 2319 . 2028

. 1769 . 1640 . 1888 . 1163 . 1016

0.3484 .3459 .3388 .3273 .3121

. 2988 . 2733 . 2515 . 2299 . 2071

. 1857 . 1655 . 1467 . 1295 . 1139

. 0998 . 0671 . 0758 . 0659 . 0578

0.991 Mov

0, 2848 - 2831 - 2780 - 2697 - 2588

. 2453 . 2302 . 2140 . 1972 . 1902

. 1638 . 1477 . 1825 . 1184 . 1053

. 0982 . 0922 . 0728 . 0686 . 0502

0. 4682 - 4658 - 4577 - 4450 - 4280

. 1669 . 1489 . 1826 . 1182 . 1060

, 1664 - 1498 - 1348 - 1215 - 1100

Angle

deg 0, 5,0 10,0 15,0 20,0

25.0 80.0 85.0 40.0 46.0

50.0 65.0 80.0 85.0 70.0

0. 4400 . 4385 . 4283 . 4097 . 3879

. 3819 . 3330 . 3026 . 2717 . 2416

.2131 .1888 .1680 .1418 .1230

.1088 .0922 .0797 .0669 .0600

| elastic scattering tinued | | | | | | | | | |
|------------------------------|---------|--|--|--|--|--|--|--|--|
| 0.853 | 0.784 | | | | | | | | |
| Mev | Mev | | | | | | | | |
| 0. 4682 | 0, 4299 | | | | | | | | |
| - 4658 | , 4277 | | | | | | | | |
| - 4577 | , 4211 | | | | | | | | |
| - 4450 | , 4104 | | | | | | | | |
| - 4280 | , 3960 | | | | | | | | |
| . 4074 | . 8786 | | | | | | | | |
| . 3842 | . 3588 | | | | | | | | |
| . 3590 | . 3872 | | | | | | | | |
| . 3828 | . 3148 | | | | | | | | |
| . 3063 | . 2916 | | | | | | | | |
| . 2801 | - 2686 | | | | | | | | |
| . 2549 | - 2480 | | | | | | | | |
| . 2906 | - 2744 | | | | | | | | |
| . 2078 | - 2088 | | | | | | | | |
| . 1865 | - 1844 | | | | | | | | |

Table 1.—Angular distribution of neutron elastic scattering for calcium (barns/steradian)—Continued

| Aogle | I. 480 Mey | f. 340 Mev | 1. 210 Mey | 1.096 May | 0.991 Mev | 0.858 Mev | 9.734 Met |
|---------------|---------------|---------------|---------------|--------------|-----------------|--------------|--------------|
| deg 100. 0 | . 0680 | .0902 | . 0617 | . 0511 | .0608 | .0961 | . 1007 |
| 105.0 | . ОНВИ | 0824 | . 0486 | 0165 | .0481 | .0899 | 0987 |
| 1100 | 0464 | 0790 | .0448 | ,0441 | . 0 48 7 | .0847 | . 0894 |
| 115.0 | .0478 | .0805 | .0447 | . 044L | .0486 | . 0839 | . 0878 |
| 150.0 | .0521 | .0676 | .0490 | .0467 | .0456 | .0886 | . 0896 |
| 126.0 | .0608 | . 1003 | . 0542 | . 0619 | . 0499 | .0980 | . 0987 |
| 180.0 | .0720 | . 1188 | . (464 | . 0698 | . 0565 | . 1028 | 1010 |
| 135-0 | . 0972 | . 1426 | . 0752 | . 0699 | . 0652 | - 1167 | . 1108 |
| 140.0 | . 1051 | . 1709 | .0993 | . 0820 | . 0755 | . 1312 | . 1227 |
| 145-0 | . 1250 | - 2023 | .10479 | . 0966 | .0969 | . 1484 | . 1360 |
| 160.0 | . 1459 | - 2362 | 1212 | . 1096 | .0090 | . 1686 | . 1501 |
| 155-0 | 1666 | - 2977 | 1373 | - 1234 | , 1109 | - 1844 | . 1640 |
| 160-0 | 1858 | -2978 | .1028 | . 1363 | . 1218 | .2010 | . 1768 |
| 165-0 | 20722 | . 3238 . | 1651 | - 1478 | 1213 | .2162 | 1879 |
| 170.0 | .2148 | . 8485 | . 1749 | . 1657 | . 1284 | . 2281 | 1983 |
| 176-0 | - 2228 | . 8560 | . 1810 | 1610 | 1429 | . 2329 | . 2016 |
| 180.0 | - 2255 | . 3602 | . 1831 | . 1628 | . 1448 | . 2352 | . 2084 |

TABLE 2. Legendre coefficients for calcium elastic scatterina

| TABLE | 2. Lege | ndre coeffi | cients for | calcium ele | ustic scatte | ring | |
|---|---|--|---|--|---|---|--|
| Energy Mev. Total elsetic berns $S_2(E) \downarrow = 0$ 1 2 4 5 6 | 18,000 0,836 1,0000 0,80316 .5346 .52043 .4496b .29692 .33349 | 17, 160 0, 828 1, 00000 0, 79842 - 63283 - 32073 - 44827 - 38273 - 32659 | 16, 300 0, 606 1, 0000 0, 77512 81067 , 50234 43006 36377 , 30684 | 16, 600 0, 707 1, 00000 0, 75672 60712 49179 41843 34726 29195 | 14, 750 0, 800 1, 00000 0, 74239 38931 48878 40920 33298 27827 | 14.000 0.804 1.00000 0.74200 74204 49053 40525 22239 38353 | 13, 300 0, 827 1, 00000 6, 72303 56333 48014 38384 29412 23372 |
| 7 | .27467 .19746 .11879 .04970 .01888 .00600 .00176 .00048 | .284,99 .182,99 .10103 .04123 .01441 .00448 .00125 .00028 | , 24861 18280 06847 03233 -01021 -00294 -00078 -00004 | . 22811 . 16236 . 07360 . 02535 . 00197 . 00048 . 00011 . 00002 | .20948 .12222 .06212 .02005 .00136 .00031 .00007 | . 1990L . 10318 . 05072 . 015772 . 0040L . 00098 . 0002L . 00004 | .16411 .07932 .04016 .01149 .00087 .00059 .00012 .00002 |
| Energy Mev— Total elastic barns St(E) l = 0 | 12,700 0,941 1,00000 0,72659 58770 47996 57652 27959 | 12, 100 0, 882 1, 00000 0, 71220 57896 48337 34800 24550 | 11, 500 0, 912 1, 00000 0, 72014 , 58101 , 45736 , 93140 , 22538 , 18944 | 10.900 0.951 1.60007 0.72907 .58442 .44935 .31296 .20430 | 10, 400 1, 030 1, 00000 0, 72052 , 67158 , 42450 , 27892 , 16765 , 11804 | 9, 890 1, 682 1, 60000 0, 72869 , 67826 , 41610 , 26968 , 16823 | 9, 410 1, 177 1, 00000 0, 78597 57503 , 90590 , 24144 , 13010 |
| 7. 8. 9. 10. 11. 12. 13. 14. | . 14672 . 08418 . 09184 . 00889 . 00197 . 00042 . 00002 | .11953 .04400 .02328 .00607 .00123 .00094 | . 10163 . 03236 . 01885 . 00428 . 00084 . 00008 | . 08462 . 67205 . 01129 . 00285 . 00054 . 00002 | .08413 .01255 .00748 .00179 .00031 .00005 | .05288 .00496 .00496 .00117 .00220 .00308 | .04149 .00621 .00630 .00076 .00012 .00002 |
| Energy Mev. Total elastic Jorna $S_t(E) J = 0$ 2 3 4 5 | 8 980 1 238 1 00000 0 74212 57477 30604 22586 11686 (06001 | 8. 510 T. 341 1. 00000 0. 74199 - 66809 - 37741 - 20825 - 09379 - 03333 - 02518 | 8. 100 1. 407 1. 00700 0. 74508 . 06447 . 36886 . 19213 . 08670 . 04620 | 1. 100 L 1823 L 00000 0. 74309 - 538306 - 39537 - 97775 - 07400 - 03236 - 01597 | 1. 561 1. 00000 0. 74353 . 65568 . 34628 . 16886 . 06757 . 02998 | 1. 709 1. 00000 0. 79635 - 54614 - 39352 - 15474 - 05690 - 02295 | 0. 004 1. 777 1. 00000 0. 73453 . 54279 . 32556 . 14743 . 05223 . 01961 |
| 7 | . 03407 . 00340 . 00315 . 00049 j . 00003 . 00001 | . 00188 . 00128 . 00027 . 00004 | . 02073 . 00119 . 00083 . 00017 . 00003 | .00055 .00050 .00011 .00002 | . 01319 . 00043 . 00033 . 00007 . 00001 | . 01015 . 00018 . 00019 . 00004 | . 00013 . 00012 . 00002 |
| Energy Mev Total elastio barns $S_l(E)$, $l = 0$ 1 2 3 4 5 6 7 8 9 | 1. 304 1. 944 1. 00000 0. 73165 53906 51721 14042 04818 01690 00062 00014 | 0.000 1.965 L.00000 0.72296 .52817 .30341 .12812 .06950 .01218 .00491 .00003 | 5, 700 2, 057 1, 00000 0, 70672 , 61546 , 28995 , 11992 , 08671 , 01029 , 00897 , 00004 | 2. 198 1.00000 0. 68561 .49904 .27561 .11108 .63080 .00709 | 5. 100 2. 818 1. 00000 0. 65982 48011 25893 10245 . 02742 . 00669 . 00240 . 00003 | 2, 972 1,00000 0, 62706 47289 24041 08839 02837 00181 00022 | 4.670 2.588 1.00000 0.61458 .46532 .22508 .05943 .02113 .00506 .00147 .00723 |
| 9 10 | .00008 | .00004 .00001 | .00008 | .00002 | .00001 | .0022 | , DATE |

Table 2. Legendre coefficients for calcium elastic scattering—Continued

| Rucray May Total elastic barns $S_{\ell}(E) I = 0$ | 4. 440 2. 669 1. 00000 0. 60352 46321 21764 - 14036 - 01835 | 4. 230 2. 761 1. 00000 0. 57103 . 44195 . 20300 . 01518 . 00376 | 4, 025 2, 868 1, 00000 0, 54777 48012 18866 07840 01416 | 3, 820 2, 955 1, 00000 0, 52006 42000 17891 07496 (1204 | 3.640 3.043 1.00000 0.60422 29063 26300 07244 01061 | 3, 460 3, 140 1, 00000 0, 47943 - 39623 - 14962 - 00755 - 00685 | 2, 290 2, 491 1, 00000 0, 42679 26934 12322 06291 00701 |
|--|---|--|---|---|--|--|--|
| Total elastia barns Sz(E) = 0 | 2. 970 8. 502 1. 00000 0. 39588 85690 10885 05815 | . 00067 . 00026 2. 690 8. 551 1. 00000 0. 36179 . 33340 . 08494 . 05179 . 00368 | 2 440 2 475 1 0000 0 34088 31843 08471 04686 00281 | 2, 210 3, 432 1, 00000 0, 31384 30156 04877 04314 00177 | 2,000 3,571 1,0000 0,28852 29452 03159 08978 00019 | 1. 810 3. 228 1. 00000 0. 22864 28741 01740 08478 00078 | 1, 630 3, 065 1, 0000 0, 2656 25148 00559 03123 .00049 |
| 6 | .00587 .00012 1,490 1,727 1,0000 0,25421 -23576 -00221 -02895 ,00031 | .00186 .00007 1.340 2.779 1.00000 0.25235 .22312 00704 .02480 .00020 | 1, 210 1, 500 1, 600 0, 25450 20742 -, 01000 0, 02103 ,00012 | 1.096 1.426 1.426 1.0000 0.22701 19271 -01179 -01784 -00006 | 0,991 1,322 1,00000 0,26074 17091 -,01599 | 0. 883 2. 303 1. 00000 0. 23830 1. 3980 01130 | 0. 724 2. 224 1. 00000 0. 224522 1.2624 —, 00044 , 01028 |

Conclusions

Reasonably satisfactory average cross section predictions for calcium at neutron energies below 18 Mey can be made with the nuclear optical model using compound elastic scattering cross sections as calculated from the optical model in the absence of inelastic scattering, and using a Hauser-Feshbach calculation if inelastic scattering is present. In order to achieve the goal of calculation of any neutron cross section as required, Hauser-Feshbach and direct interaction inelastic scattering codes for inelastic scattering, and nuclear reaction codes will be required, for which the present type of calculation provides input data.

More experimental data in the region from 6 to 14 Mey is needed. Also the difference between the Seagrave et al. and the Lane et al. data at low

energies needs to be resolved.

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